

**TITLE OF INVENTION**

CURABLE BASE-RESISTANT FLUOROELASTOMERS

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**CROSS-REFERENCE TO RELATED APPLICATIONS**

This application is a division of application Serial No. 10/137,914 filed May 2, 2002 which claims priority to provisional application No. 60/290,900, filed May 15, 2001.

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**FIELD OF THE INVENTION**

This invention relates to polyhydroxy curable fluoroelastomer compositions wherein the fluoroelastomer comprises copolymerized units of tetrafluoroethylene, propylene, and a cure site monomer selected from the group consisting of i) trifluoroethylene, ii) 3,3,3-trifluoropropene-1, iii) 1,2,3,3,3-pentafluoropropylene, iv) 1,1,3,3,3-pentafluoropropylene, and v) 2,3,3,3-tetrafluoropropene.

**BACKGROUND OF THE INVENTION**

Specialty fluoroelastomers made from copolymers of tetrafluoroethylene (TFE), propylene (P), and optionally vinylidene fluoride (VF<sub>2</sub>) (i.e. TFE/P dipolymers or VF<sub>2</sub>/TFE/P terpolymers) are often utilized in applications wherein resistance to alkaline fluids and other high pH chemicals is critical. The TFE/P dipolymers have the best resistance to alkaline fluids. Terpolymers containing more than about 10 wt.% vinylidene fluoride units generally do not have significantly better alkaline fluid resistance than do conventional fluoroelastomers made from copolymers of vinylidene fluoride, hexafluoropropylene and tetrafluoroethylene.

In order to fully develop physical properties such as tensile strength, elongation, and compression set, elastomers must be cured, i.e. crosslinked. In the case of fluoroelastomers, this is generally accomplished by mixing uncured polymer (i.e. fluoroelastomer gum) with a polyfunctional curing agent and heating the resultant mixture under pressure, thereby promoting chemical reaction of the curing agent with

active sites along the polymer backbone or side chains. Interchain linkages produced as a result of these chemical reactions cause formation of a crosslinked polymer composition having a three-dimensional network

5 structure. Commonly used curing agents for fluoroelastomers include difunctional nucleophilic reactants, such as polyhydroxy compounds. Alternatively, peroxidic curing systems containing organic peroxides and unsaturated coagents, such as polyfunctional isocyanurates, may be employed.

10 In many cases, polyhydroxy and peroxide cure processes or curing agent formulations are unsatisfactory when used to crosslink these specialty fluoroelastomers. For example, it is known to cure elastomeric VF<sub>2</sub>/TFE/P terpolymers with either peroxide (U.S. Patent No. 4,910,260) or polyhydroxy (U.S. Patent Nos. 4,882,390 and 4,912,171) cure systems.

15 However, when such compositions are cured using a polyhydroxy compound, the cured products may exhibit undesirably high compression set. In fact, such specialty fluoroelastomers which contain less than about 10 wt.% copolymerized units of vinylidene fluoride show little to no cure response with polyhydroxy cure formulations.

20 The peroxide cures disclosed in U.S. Patent 4,910,260 are undesirable because the curable compositions which are initially formed are extremely scorchy and would therefore be unsuitable for many commercial processes.

It would be particularly desirable to have an improved specialty

25 fluoroelastomer that is resistant to alkaline fluids and which readily crosslinks with polyhydroxy cure systems to form cured articles having good tensile properties and compression set resistance.

#### SUMMARY OF THE INVENTION

30 It has been surprisingly found that the incorporation of a cure site monomer selected from the group consisting of i) trifluoroethylene, ii) 3,3,3-trifluoropropene-1, iii) 1,2,3,3,3-pentafluoropropylene, iv) 1,1,3,3,3-

pentafluoropropylene, and v) 2,3,3,3-tetrafluoropropene into TFE/P dipolymers or into VF<sub>2</sub>/TFE/P terpolymers improves the polyhydroxy curing of these specialty fluoroelastomers without significantly diminishing the

5 resistance of these fluoroelastomers to alkaline fluids. The resulting cured fluoroelastomer articles have excellent compression set resistance and tensile properties.

Accordingly, an aspect of this invention is a curable fluoroelastomer composition comprising

10           A) a specialty fluoroelastomer comprising copolymerized units of 45 to 80 weight percent tetrafluoroethylene; 10 to 40 weight percent propylene; and 0.1 to 15 weight percent of a cure site monomer selected from the group consisting of i) trifluoroethylene, ii) 3,3,3-trifluoropropene-1, iii) 1,2,3,3,3-pentafluoropropylene, iv) 1,1,3,3,3-pentafluoropropylene, and v) 2,3,3,3-tetrafluoropropene;

15           B) 0.1 to 20 parts by weight per 100 parts fluoroelastomer of a polyhydroxy curing agent;

              C) 1 to 30 parts by weight per 100 parts fluoroelastomer of an acid acceptor; and

20           D) 0.1 to 20 parts by weight per 100 parts fluoroelastomer of a vulcanization accelerator.

The polyhydroxy curing agent and vulcanization accelerator may be present as separate components or as the salt of the curing agent and accelerator.

25           Another aspect of the present invention is a specialty fluoroelastomer comprising copolymerized units of 45 to 80 weight percent tetrafluoroethylene; 10 to 40 weight percent propylene; and 0.1 to 15 weight percent of 3,3,3-trifluoropropene-1 cure site monomer.

30           **DETAILED DESCRIPTION OF THE INVENTION**

Specialty fluoroelastomers which may be employed in the curable compositions of this invention include the terpolymer of tetrafluoroethylene

(TFE), propylene (P) and a cure site monomer selected from the group consisting of i) trifluoroethylene (TrFE), ii) 3,3,3-trifluoropropene-1 (TFP),  
iii) 1,2,3,3,3-pentafluoropropylene (1-HPFP) iv) 1,1,3,3,3-  
5 pentafluoropropylene (2-HPFP), and v) 2,3,3,3-tetrafluoropropene. Minor amounts (i.e. less than about 20 weight percent total) of other copolymerizable monomers may be present in higher order copolymer fluoroelastomers of this invention. Examples of such monomers include, but are not limited to chlorotrifluoroethylene, vinyl fluoride, perfluoro(alkyl  
10 vinyl) ethers, perfluoro(alkoxy vinyl) ethers, perfluoro(alkoxyalkyl vinyl) ethers, perfluoroalkyl- or perfluoroalkoxy- alkenyl ethers (such as those disclosed in U.S. Patent No. 5,891,965), ethylene, isobutene, and bromine- or iodine-containing cure site monomers such as  
 $\text{CF}_2=\text{CFOCF}_2\text{CF}_2\text{CF}_2\text{OCF}_2\text{CF}_2\text{Br}$ ; 1-bromo-2,2-difluoroethylene; bromo-  
15 trifluoroethylene; 4-bromo-3,3,4,4-tetrafluorobutene-1; 4-bromo-1,1,2-trifluorobutene-1; 2-bromoperfluoro(ethyl vinyl) ether; 3-bromoperfluoro(propyl vinyl) ether; and 4-iodo-3,3,4,4-tetrafluorobutene-1. Alternatively, bromine or iodine cure sites may be introduced onto the fluoroelastomer polymer chain ends by use of iodinated or brominated  
20 chain transfer agents such as methylene iodide or 1,4-diiodoperfluorobutane during polymerization. The presence of brominated or iodinated groups permits the fluoroelastomers of this invention to be cured by organic peroxides in addition to polyhydroxy curatives.

Generally the specialty fluoroelastomers used in the compositions  
25 of this invention contain between 45 to 80 (preferably between 50 to 78, most preferably 65 to 78) weight percent copolymerized units of tetrafluoroethylene, based on the total weight of the fluoroelastomer. Less TFE causes the polymerization to be slow, while more TFE causes the resulting polymer to be plastic, rather than elastomeric.

30 The fluoroelastomers employed in the compositions of this invention typically contain between 10 to 40 (preferably between 12 to 30, most preferably 15 to 25) weight percent copolymerized units of

propylene, based on the total weight of the fluoroelastomer. Less propylene causes the polymer to become plastic, while more propylene causes the polymerization to become slow.

5       The specialty fluoroelastomers used in the compositions of this invention also contain 0.1 to 15 (preferably 2 to 10, most preferably 3-6) weight percent copolymerized units of a cure site monomer, based on the total weight of the fluoroelastomer. The cure site monomer is selected from the group consisting of i) trifluoroethylene, ii) 3,3,3-trifluoropropene-1,  
10      iii) 1,2,3,3,3-pentafluoropropylene, iv) 1,1,3,3,3-pentafluoropropylene, and v) 2,3,3,3-tetrafluoropropene. The monomer 3,3,3-trifluoropropene-1 is especially preferred.

It is believed that during the polyhydroxy curing process, some copolymerized units of cure site monomer, which are located adjacent to 15 tetrafluoroethylene units in the fluoroelastomer polymer chain, dehydrofluorinate to form sites of unsaturation (i.e. C-C double bonds). These unsaturated sites are then available to react with polyhydroxy curatives to form crosslinks. Fluoroelastomers containing less than 0.1 wt.% units of cure site units do not form a sufficient number of crosslinks  
20      to yield a cured product having desirable tensile properties for most end uses. Fluoroelastomers containing more than 15 wt. % cure site units are not desirable because the polymerization is slowed and there is a reduction in the fluoroelastomer's resistance to alkaline fluids and other high pH chemicals.

25       A particularly preferred fluoroelastomer comprises copolymerized units of tetrafluoroethylene, propylene and 3,3,3-trifluoropropene-1 in the amounts specified above.

30       Preferably, the fluoroelastomers employed in this invention do not contain any copolymerized units of vinylidene fluoride. However, the fluoroelastomers may, optionally, contain up to 20 weight percent copolymerized units of vinylidene fluoride ( $\text{VF}_2$ ), based on the total weight of the fluoroelastomer. If the fluoroelastomer does contain units of

vinylidene fluoride, the level is preferably 2 to 20 (most preferably between 10 and 20) weight percent. Generally, the lower the level of vinylidene fluoride, the better the fluoroelastomer's resistance to alkaline fluids (also referred to as "base resistance" in the art). However, copolymers of TFE and P containing no vinylidene fluoride units generally have poor resistance to hydrocarbon fluids such as oils or fuels. The addition of VF<sub>2</sub> to the fluoroelastomer increases the fluorine atom content and thus improves the resistance to hydrocarbons, but at the same time reduces the resistance of the fluoroelastomer to polar fluids. Depending upon the end use application environment, fluoroelastomer base resistance and hydrocarbon fluid resistance can be balanced by adjusting the level of copolymerized vinylidene fluoride and tetrafluoroethylene in the fluoroelastomer.

The fluoroelastomers of this invention are generally prepared by free radical emulsion or suspension polymerization. Preferably, the polymerizations are carried out in batch, or semi-batch emulsion processes well known in the art. The resulting fluoroelastomer latexes are usually coagulated by addition of electrolytes. The precipitated polymer is washed with water and then dried, for example in an air oven, to produce a substantially dry fluoroelastomer gum.

In the semi-batch emulsion polymerization process of this invention, a gaseous monomer mixture of a desired composition (initial monomer charge) is introduced into a reactor which contains an aqueous solution.

The aqueous solution contains a surfactant such as ammonium perfluorooctanoate or perfluorohexylethyl sulfonic acid. Generally, the pH of the solution is controlled to between 1 and 7 (preferably 3-7), depending upon the type of fluoroelastomer being made. In addition, the initial aqueous solution may contain a nucleating agent, such as a fluoroelastomer seed polymer prepared previously, in order to promote fluoroelastomer latex particle formation and thus speed up the polymerization process.

The initial monomer charge contains a quantity of a TFE, P and cure site monomer and, optionally, one or more additional monomers such as VF<sub>2</sub>. The amount of monomer mixture contained in the initial charge is 5 set so as to result in a reactor pressure between 0.5 and 10 MPa.

The monomer mixture is dispersed in the aqueous medium and, optionally, a chain transfer agent may also be added at this point while the reaction mixture is agitated, typically by mechanical stirring.

The temperature of the semi-batch reaction mixture is maintained in 10 the range of 25°C – 130°C, preferably 50°C – 100°C. Polymerization begins when the initiator either thermally decomposes or reacts with reducing agent and the resulting radicals react with dispersed monomer.

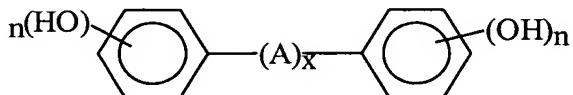
Additional quantities of the gaseous major monomers and cure site monomer (incremental feed) are added at a controlled rate throughout the 15 polymerization in order to maintain a constant reactor pressure at a controlled temperature.

Polymerization times in the range of from 2 to 60 hours are typically employed in this semi-batch polymerization process.

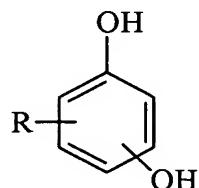
Curable compositions of this invention contain 1) a specialty 20 fluoroelastomer, as defined above, (preferably the fluoroelastomer of this invention), 2) a polyhydroxy curative, 3) an acid acceptor and 4) a vulcanization (or curing) accelerator. In the case of fluoroelastomers which contain bromine or iodine atom cure sites, the curable compositions of this invention may, optionally, also contain an organic peroxide and a 25 multifunctional curing coagent. Cured articles resulting from the latter compositions contain crosslinks due to both the polyhydroxy and peroxide curing systems and are sometimes referred to in the art as dual cured elastomers.

The curable compositions of the invention contain between 0.1 to 30 20 parts by weight (preferably 1-3 parts) of polyhydroxy crosslinking agent (or a derivative thereof) per 100 parts fluoroelastomer. Typical polyhydroxy cross-linking agents include di-, tri-, and

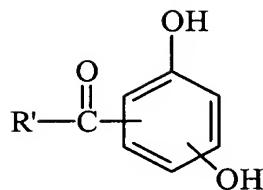
tetrahydroxybenzenes, naphthalenes, and anthracenes, and bisphenols of the formula



where A is a difunctional aliphatic, cycloaliphatic, or aromatic radical of 1-13 carbon atoms, or a thio, oxy, carbonyl, sulfinyl, or sulfonyl radical; A may optionally be substituted with at least one chlorine or fluorine atom; x is 0 or 1; n is 1 or 2; and any aromatic ring of the polyhydroxylic compound may optionally be substituted with at least one chlorine or fluorine atom, an amino group, a -CHO group, or a carboxyl or acyl radical. Preferred polyhydroxy compounds include hexafluoroisopropylidene-bis(4-hydroxy-benzene) (i.e. bisphenol AF or BPAF); 4,4'-isopropylidene diphenol (i.e. bisphenol A); 4,4'-dihydroxydiphenyl sulfone; and diaminobisphenol AF. Referring to the bisphenol formula shown above, when A is alkylene, it can be for example methylene, ethylene, chloroethylene, fluoroethylene, difluoroethylene, propylidene, isopropylidene, tributylidene, heptachlorobutylidene, heptafluorobutylidene, pentylidene, hexylidene, and 1,1-cyclohexylidene. When A is a cycloalkylene radical, it can be for example 1,4-cyclohexylene, 2-chloro-1,4-cyclohexylene, cyclopentylene, or 2-fluoro-1,4-cyclohexylene. Further, A can be an arylene radical such as m-phenylene, p-phenylene, o-phenylene, methylphenylene, dimethylphenylene, 1,4-naphthylene, 3-fluoro-1,4-naphthylene, and 2,6-naphthylene. Polyhydroxyphenols of the formula



or



where R is H or an alkyl group having 1-4 carbon atoms or an aryl group containing 6-10 carbon atoms and R' is an alkyl group containing 1-4

5     carbon atoms also act as effective crosslinking agents. Examples of such compounds include hydroquinone, catechol, resorcinol, 2-methylresorcinol, 5-methyl-resorcinol, 2-methylhydroquinone, 2,5-dimethylhydroquinone, 2-t-butyl-hydroquinone; and such compounds as 1,5-dihydroxynaphthalene and 2,6-dihydroxynaphthalene.

10      Additional polyhydroxy curing agents include alkali metal salts of bisphenol anions, quaternary ammonium salts of bisphenol anions, tertiary sulfonium salts of bisphenol anions and quaternary phosphonium salts of bisphenol anions. For example, the salts of bisphenol A and bisphenol AF. Specific examples include the disodium salt of bisphenol AF, the dipotassium salt of bisphenol AF, the monosodium monopotassium salt of bisphenol AF and the benzyltriphenylphosphonium salt of bisphenol AF.

15      Quaternary ammonium and phosphonium salts of bisphenol anions are discussed in U.S. Patents 4,957,975 and 5,648,429. Bisphenol AF salts (1:1 molar ratio) with quaternary ammonium ions of the formula

20       $\text{R}_1\text{R}_2\text{R}_3\text{R}_4\text{N}^+$ , wherein  $\text{R}_1-\text{R}_4$  are  $\text{C}_1\text{-C}_8$  alkyl groups and at least three of  $\text{R}_1-\text{R}_4$  are  $\text{C}_3$  or  $\text{C}_4$  alkyl groups are preferred. Specific examples of these preferred compositions include the 1:1 molar ratio salts of tetrapropyl ammonium-, methyltributylammonium- and tetrabutylammonium bisphenol AF. Such salts may be made by a variety of methods. For instance a

25      methanolic solution of bisphenol AF may be mixed with a methanolic solution of a quaternary ammonium salt, the pH is then raised with sodium methoxide, causing an inorganic sodium salt to precipitate. After filtration, the tetraalkylammonium/BPAF salt may be isolated from solution by evaporation of the methanol. Alternatively, a methanolic solution of

tetraalkylammonium hydroxide may be employed in place of the solution of quaternary ammonium salt, thus eliminating the precipitation of an inorganic salt and the need for its removal prior to evaporation of the  
5 solution.

In addition, derivatized polyhydroxy compounds such as mono- or diesters, and trimethylsilyl ethers are useful crosslinking agents.  
Examples of such compositions include, but are not limited to resorcinol monobenzoate, the diacetate of bisphenol AF, the diacetate of sulfonyl  
10 diphenol, and the diacetate of hydroquinone.

The curable compositions of the invention also contain between 1 to 30 parts by weight (preferably 1 to 7 parts) of an acid acceptor per 100 parts fluoroelastomer. The acid acceptor is typically a strong organic base such as Proton Sponge® (available from Aldrich) or an oxirane, or an  
15 inorganic base such as a metal oxide, metal hydroxide, or a mixture of 2 or more of the latter. Metal oxides or hydroxides which are useful acid acceptors include calcium hydroxide, magnesium oxide, lead oxide, zinc oxide and calcium oxide. Calcium hydroxide and magnesium oxide are preferred.

20 Vulcanization accelerators which may be used in the curable compositions of the invention include tertiary sulfonium salts such as  $[(C_6H_5)_2S^+(C_6H_{13})][Cl^-]$ , and  $[(C_6H_{13})_2S(C_6H_5)]^+[CH_3CO_2^-]$  and quaternary ammonium, phosphonium, arsonium, and stibonium salts of the formula  $R_5R_6R_7R_8Y^+ X^-$ , where Y is phosphorous, nitrogen, arsenic, or antimony;  
25 R<sub>5</sub>, R<sub>6</sub>, R<sub>7</sub>, and R<sub>8</sub> are individually C<sub>1</sub>-C<sub>20</sub> alkyl, aryl, aralkyl, alkenyl, and the chlorine, fluorine, bromine, cyano, -OR, and -COOR substituted analogs thereof, with R being C<sub>1</sub>-C<sub>20</sub> alkyl, aryl, aralkyl, alkenyl, and where X is halide, hydroxide, sulfate, sulfite, carbonate, pentachlorothiophenolate, tetrafluoroborate, hexafluorosilicate,  
30 hexafluorophosphate, dimethyl phosphate, and C<sub>1</sub>-C<sub>20</sub> alkyl, aryl, aralkyl, and alkenyl carboxylates and dicarboxylates. Particularly preferred are benzyltri-phenylphosphonium chloride, benzyltriphenylphosphonium

bromide, tetrabutylammonium hydrogen sulfate, tetrabutylammonium hydroxide, tetrapropylammonium hydroxide, tetrabutylammonium bromide, tributylallylphosphonium chloride, tributyl-2-methoxypropylphosphonium chloride, 1,8-diazabicyclo[5.4.0]undec-7-ene, and benzylidiphenyl(dimethylamino) phosphonium chloride. Other useful accelerators include methyltriocetyl ammonium chloride, methyltributylammonium chloride, tetrapropylammonium chloride, benzyltriocetylphosphonium bromide, benzyltriocetylphosphonium chloride, 10 methyltriocetylphosphonium acetate, tetraoctylphosphonium bromide, methyltriphenylarsonium tetrafluoroborate, tetraphenylstibonium bromide, 4-chlorobenzyltriphenyl phosphonium chloride, 8-benzyl-1,8-diazabicyclo(5.4.0)-7-undecenonium chloride, diphenylmethyltriphenylphosphonium chloride, allyltriphenyl-phosphonium chloride, tetrabutylphosphonium bromide, m-trifluoromethylbenzyltriocetylphosphonium chloride, and other quaternary compounds disclosed in U.S. Patent Nos. 5,591,804; 4,912,171; 4,882,390; 4,259,463; 4,250,278 and 3,876,654. The amount of accelerator used is between 0.1 and 20 parts by weight per hundred parts by weight fluoroelastomer.

20 Preferably, 0.5-3.0 parts accelerator per hundred parts fluoroelastomer is used.

Optionally, the curable compositions of the invention may contain a second curing agent in the form of a combination of an organic peroxide and a multifunctional (i.e. polyunsaturated) coagent compound. Examples 25 of organic peroxides which are particularly effective curing agents for fluoroelastomers include dialkyl peroxides or bis(dialkyl peroxides) which decompose at a temperature above 50°C. In many cases one will prefer to use a di-t-butylperoxide having a tertiary carbon atom attached to a peroxy oxygen. Among the most useful are 2,5-dimethyl-2,5-di(t-butylperoxy)hexyne-3 and 2,5-dimethyl-2,5-di(t-butyl-peroxy)hexane. 30 Other peroxides can be selected from such compounds as dicumyl peroxide, dibenzoyl peroxide, t-butyl perbenzoate, and di[1,3-dimethyl-3-(t-

butyl-peroxy)butyl]carbonate. Multifunctional coagents which cooperate with such peroxides to provide curing systems include methacrylates, allyl compounds, divinyl compounds, and polybutadienes. Specific examples

5      of coagents include one or more of the following compounds: triallyl cyanurate; triallyl isocyanurate; tris(diallylamine-s-triazine); triallyl phosphite; hexaallyl phosphoramide, N,N-diallyl acrylamide; N,N,N'N'-tetraallyl terephthalamide; N,N,N',N'-tetraallyl malonamide; trivinyl isocyanurate; 2,4,6-trivinylmethyltrisiloxane; and tri(5-norbornene-2-

10     methylene)cyanurate. If a peroxide cure system is present in the compounds of the invention, the organic peroxide is generally at a level between 0.2 to 7 parts by weight (preferably 1 to 3 parts) per 100 parts fluoroelastomer and the coagent is present at a level of 0.1 to 10 (preferably 2 to 5) parts by weight per 100 parts fluoroelastomer.

15     The curable composition of the invention may contain other additives, commonly used in elastomer compounding and processing. The latter may be introduced into the composition before addition of the curative, simultaneously with it, or following the addition. Typical additives include fillers, plasticizers, processing aids, antioxidants, pigments, and

20     the like. The amount of such ingredients which is added will depend on the particular end use applications for which the cured compositions are adapted. Fillers, such as carbon black, clays, barium sulfate, calcium carbonate, magnesium silicate, and fluoropolymers are generally added in amounts of from 5-100 parts by weight per 100 parts fluoroelastomer. The

25     amount of plasticizer used is generally from 0.5-5.0 parts by weight per 100 parts fluoroelastomer. Typical plasticizers include esters, such as dioctyl phthalate and dibutyl sebacate. Processing aids are generally used in amounts of from 0.1-2.0 parts by weight per 100 parts fluoroelastomer. Suitable processing aids include octadecylamine,

30     tetramethylene sulfone, p-chlorophenyl sulfone, and waxes, for example, carnauba wax, that aid in the processing of the compositions.

The fluoroelastomer, polyhydroxy curative, acid acceptor, accelerator and any other ingredients are generally incorporated into the curable compositions of the invention by means of an internal mixer or  
5 rubber mill. The resulting composition may then be shaped (e.g. molded or extruded) and cured. Curing typically takes place at about 150°-200°C for 1 to 60 minutes. Conventional rubber curing presses, molds, extruders, and the like provided with suitable heating and curing means can be used. Also, for optimum physical properties and dimensional  
10 stability, it is preferred to carry out a post curing operation wherein the molded or extruded article is heated in an oven or the like for an additional period of about 1-48 hours, typically from about 180°-275°C, generally in an air atmosphere.

The polymers of the invention and curable compositions of the  
15 invention result in cured fluoroelastomer articles which have unusually good base resistance, tensile properties and compression set resistance. Such articles find application as gaskets, seals and tubing, particularly in automotive end uses.

The invention is now illustrated by the following embodiments in  
20 which all parts are by weight unless otherwise indicated.

### EXAMPLES

#### Test Methods

Physical properties of the compositions described in the  
25 examples were measured according to the following test procedures.

Mooney Scorch	ASTM D1646
Oscillating Disc Rheometer (ODR)	ASTM D2084
Moving Disc Rheometer (MDR)	ASTM D5289
Tensile Strength ( $T_B$ )	ASTM D412
30 Modulus ( $M_{100}$ )	ASTM D412
Elongation at Break ( $E_B$ )	ASTM D412
Hardness	ASTM D2240
Compression Set-B	ASTM D395

Example 1

A polymer of the invention (Polymer 1) was prepared by a semi-batch emulsion polymerization, carried out at 60°C in a well-stirred reaction vessel. A 33-liter, horizontally agitated reactor was charged with 20 liters of deionized, deoxygenated water, 150 g of ammonium perfluorooctanoate and 70 g of sodium phosphate dibasic heptahydrate. The reactor was heated to 60°C and then pressurized to 1.93 MPa with a mixture of 80.0 wt.% tetrafluoroethylene (TFE), 10.0 wt.% propylene (P), and 10.0 wt.% 3,3,3-trifluoropropene-1 (TFP). A 250 ml aliquot of an aqueous 10 wt.% ammonium persulfate initiator solution was then added. A mixture of 70.0 wt.% TFE, 20.0 wt.% P, and 10.0 wt.% TFP was supplied to the reactor to maintain a pressure of 1.93 MPa throughout the polymerization. The initiator solution was fed continuously at 5 ml/hour through the end of the reaction period. After a total of 6000 g of monomer mixture had been supplied to the reactor, monomer addition was discontinued and the reactor was purged of residual monomer. The total reaction time was 60 hours. The resulting fluoroelastomer latex was coagulated by addition of aluminum potassium sulfate solution, filtered and then washed with deionized water. The polymer crumb was dried for two days at 60°C. The product, composed of 70 wt.% TFE units, 20 wt.% P units, and 10 wt.% TFP units, was an amorphous elastomer having a glass transition temperature of 8°C, as determined by differential scanning calorimetry (heating mode, 10°C/minute, inflection point of transition).

Mooney viscosity, ML-10 (121°C), was 19.

Example 2

A polymer of the invention (Polymer 2) was prepared by a semi-batch emulsion polymerization, carried out at 60°C in a well-stirred reaction vessel. A 33-liter, horizontally agitated reactor was charged with 20 liters of deionized, deoxygenated water, 300 g of ammonium perfluorooctanoate and 70 g of sodium phosphate dibasic heptahydrate.

The reactor was heated to 60°C and then pressurized to 2.07 MPa with a mixture of 90.0 wt.% TFE, 5.0 wt.% P, and 5.0 wt.% TFP. A 250 ml aliquot of an aqueous 10 wt.% ammonium persulfate initiator solution was 5 then added. A mixture of 73.0 wt.% TFE, 23.0 wt.% P, and 4.0 wt.% TFP was supplied to the reactor to maintain a pressure of 2.07 MPa throughout the polymerization. The initiator solution was fed continuously at 5 ml/hour through the end of the reaction period. After a total of 8000 g monomer mixture had been supplied to the reactor, monomer addition was 10 discontinued and the reactor was purged of residual monomer. The total reaction time was 36 hours. A portion of the resulting fluoroelastomer latex was retained for use as a seed polymer latex in Example 4. The remaining latex was coagulated by addition of aluminum potassium sulfate solution and then washed with deionized water. The polymer crumb was 15 dried for two days at 60°C. The product, containing 73 wt.% TFE units, 23 wt.% P units, and 4 wt.% TFP units, was an amorphous fluoroelastomer having a glass transition temperature of 0.3°C, as determined by differential scanning calorimetry (heating mode, 10°C/minute, inflection point of transition). Mooney viscosity, ML-10 (121°C), was 17.

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Example 3

A polymer of the invention (Polymer 3) was prepared by a semi-batch emulsion polymerization, carried out at 60°C in a well-stirred reaction vessel. A 33-liter, horizontally agitated reactor was charged with 25 20 liters of deionized, deoxygenated water, 200 g of perfluorohexylethyl sulfonic acid and 20 g of sodium hydroxide. The reactor was heated to 60°C and then pressurized to 2.07 MPa with a mixture of 95.0 wt.% TFE and 5.0 wt.% P. A 326 ml aliquot of an aqueous initiator solution containing 10 wt.% ammonium persulfate and 2.5 wt.% sodium hydroxide 30 was then added. A mixture of 70.0 wt.% TFE, 20.0 wt.% P, 5.0 wt.% vinylidene fluoride (VF<sub>2</sub>), and 5.0 wt.% TFP was supplied to the reactor to maintain a pressure of 2.07 MPa throughout the polymerization. The

initiator solution was fed continuously at 6 ml/hour through the end of the reaction period. After a total of 8000g monomer mixture had been supplied to the reactor, monomer addition was discontinued and the 5 reactor was purged of residual monomer. The total reaction time was 25 hours. The resulting fluoroelastomer latex was coagulated by addition of aluminum potassium sulfate solution and then washed with deionized water. The polymer crumb was dried for two days at 60°C. The product, containing 70 wt.% TFE units, 20 wt.% P units, 5 wt.% VF<sub>2</sub>, and 5 wt.% 10 TFP units, had a Mooney viscosity, ML-10 (121°C), of 21.

Example 4

A polymer of the invention (Polymer 4) was prepared by a semi-batch emulsion polymerization process, carried out at 60°C in a well-stirred reaction vessel. A 33-liter, horizontally agitated reactor was charged with 17.4 liters of deionized, deoxygenated water, 259 g of ammonium perfluorooctanoate, 70 g of sodium phosphate dibasic heptahydrate and 4000 g of seed polymer latex from Example 2. The reactor was heated to 60°C and then pressurized to 2.07 MPa with a 15 mixture of 95.0 wt.% TFE and 5.0 wt.% P. A 225 ml aliquot of an aqueous 10 wt.% ammonium persulfate initiator solution was then added. A mixture of 73.0 wt.% TFE, 23.0 wt.% P, and 4.0 wt.% TFP was supplied to the reactor to maintain a pressure of 2.07 MPa throughout the polymerization. The initiator solution was fed continuously at 5 ml/hour 20 through the end of the reaction period. After a total of 6800 g monomer mixture had been supplied to the reactor, monomer addition was discontinued and the reactor was purged of residual monomer. The total 25 reaction time was 19 hours. The resulting fluoroelastomer latex was coagulated by addition of aluminum potassium sulfate solution and then washed with deionized water. The polymer crumb was dried for two days at 60°C. The product, composed of 73 wt.% TFE units, 23 wt.% P units, 30 and 4 wt.% TFP units, was an amorphous fluoroelastomer having a glass

transition temperature of 3°C, as determined by differential scanning calorimetry (heating mode, 10°C/minute, inflection point of transition). Mooney viscosity, ML-10 (121°C), was 23.

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Control A

A seed polymer latex was prepared by a semi-batch emulsion polymerization process, carried out at 60°C in a well-stirred reaction vessel. A 33-liter, horizontally agitated reactor was charged with 20 liters 10 of deionized, deoxygenated water, 300 g of ammonium perfluorooctanoate and 90 g of sodium phosphate dibasic heptahydrate. The reactor was heated to 60°C and then pressurized to 2.07 MPa with a mixture of 75.0 wt.% TFE, 5.0 wt.% P, and 20.0 wt.% VF<sub>2</sub>. A 250 ml aliquot of an aqueous 10 wt.% ammonium persulfate initiator solution was then added. 15 A mixture of 70.0 wt.% TFE, 20.0 wt.% P, and 10.0 wt.% VF<sub>2</sub> was supplied to the reactor to maintain a pressure of 2.07 MPa throughout the polymerization. The initiator solution was fed continuously at 5 ml/hour through the end of the reaction period. After a total of 8000 g monomer mixture had been supplied to the reactor, monomer addition was 20 discontinued and the reactor was purged of residual monomer. The total reaction time was 30 hours. The resulting emulsion had a solids level of 32.7% and was used as seed to make a Control Polymer (Control Polymer A).

Control Polymer A was prepared by a semi-batch emulsion 25 polymerization process, carried out at 60°C in a well-stirred reaction vessel. A 33-liter, horizontally agitated reactor was charged with 16 liters of deionized, deoxygenated water, 300 g of ammonium perfluorooctanoate, 90 g of sodium phosphate dibasic heptahydrate and 4000 g of the seed polymer latex prepared above. The reactor was 30 heated to 60°C and then pressurized to 2.07 MPa with a mixture of 75.0 wt.% TFE, 5.0 wt.% P, and 20.0 wt.% VF<sub>2</sub>. A 250 ml aliquot of an aqueous 10 wt.% ammonium persulfate initiator solution was then added.

A mixture of 70.0 wt.% TFE, 20.0 wt.% P, and 10.0 wt.% VF<sub>2</sub> was supplied to the reactor to maintain a pressure of 2.07 MPa throughout the polymerization. The initiator solution was fed continuously at 5 ml/hour

5 through the end of the reaction period. After a total of 8000 g monomer mixture had been supplied to the reactor, monomer addition was discontinued and the reactor was purged of residual monomer. The total reaction time was 20 hours. The resulting emulsion was coagulated by addition of magnesium sulfate solution and then washed with deionized

10 water. The polymer crumb was dried for two days at 60°C. The product, composed of 70 wt.% TFE units, 20 wt.% P units, and 10 wt.% VF<sub>2</sub> units, was an amorphous elastomer having a glass transition temperature of 2°C, as determined by differential scanning calorimetry (heating mode, 10°C/minute, inflection point of transition). Mooney viscosity, ML-10

15 (121°C), was 46.

Example 5

Curable compositions of the invention were made by mixing some of the fluoroelastomers of the invention prepared above with a polyhydroxy

20 curative, acid acceptor, vulcanization accelerator and other ingredients on a conventional two-roll rubber mill, using standard mixing techniques employed in the elastomer industry. Comparative curable compositions were made by the same procedure except that a fluoroelastomer of the prior art (Control Polymer A), not containing TFP cure site monomer units

25 was used. The formulations are shown in Table I.

Curing characteristics were measured by ODR (at 177°C, 3° arc 24 minutes) according to the Test Methods. The results are also shown in Table I

TABLE I

Ingredient, phr <sup>1</sup>	Sample 1	Sample 2	Comp. Sample A	Sample 3	Sample 4	Comp. Sample B
Polymer 3	100	0	0	100	0	0
Polymer 4	0	100	0	0	100	0
Control Polymer A	0	0	100	0	0	100
Elastomag 170 <sup>2</sup>	4	4	4	4	4	4
Calcium hydroxide	8	8	8	8	8	8
MT carbon black	30	30	30	30	30	30
TBAHAF <sup>3</sup>	3.54	3.54	3.54			
TPAHAF <sup>4</sup>	0	0	0	3.21	3.21	3.21
<u>Curing Characteristics</u>						
M <sub>L</sub> , dN·m	7.9	4.4	10.8	6.2	4.5	9.5
M <sub>H</sub> , dN·m	53.8	51.2	34.4	88.8	82.9	56.2
t <sub>s2</sub> , minutes	2.6	4.4	1.8	4.1	9.1	4.1
tc90, minutes	13.6	19.3	7.0	10.6	20.5	7.5

<sup>1</sup> phr is parts by weight per 100 parts by weight rubber (i.e. elastomer)

5   <sup>2</sup> Magnesium oxide available from Morton Performance Chemicals, Inc.

<sup>3</sup> salt (1:1 molar ratio) of bisphenol AF curative and tetrabutylammonium hydroxide  
accelerator

<sup>4</sup> salt (1:1 molar ratio) of bisphenol AF curative and tetrapropylammonium hydroxide  
accelerator

Example 6

A seed polymer latex of the invention was prepared by a semi-batch emulsion polymerization process, carried out at 60°C in a well-stirred reaction vessel. A 33-liter, horizontally agitated reactor was charged with 20 liters of deionized, deoxygenated water, 150 g of ammonium perfluorooctanoate and 70 g of sodium phosphate dibasic heptahydrate. The reactor was heated to 60°C and then pressurized to 2.07 MPa with a mixture of 90.0 wt.% TFE, 5.0 wt.% P, and 5.0 wt.% TFP.

5       A 250 ml aliquot of an aqueous 10 wt.% ammonium persulfate initiator solution was then added. A mixture of 73.0 wt.% TFE, 24.0 wt.% P, and 3.0 wt.% TFP was supplied to the reactor to maintain a pressure of 2.07 MPa throughout the polymerization. The initiator solution was fed continuously at 5 ml/hour through the end of the reaction period. After a

10      total of 6000 g monomer mixture had been supplied to the reactor, monomer addition was discontinued and the reactor was purged of residual monomer. The total reaction time was 46 hours. The resulting emulsion had a solids content of 19 wt.% and was used as seed to make the following polymer (Polymer 5).

15      A polymer of the invention (Polymer 5) was prepared by a semi-batch emulsion polymerization process, carried out at 60°C in a well-stirred reaction vessel. A 33-liter, horizontally agitated reactor was charged with 16 liters of deionized, deoxygenated water, 450 g of ammonium perfluorooctanoate, 90 g of sodium phosphate dibasic heptahydrate and 4000 g of the seed polymer latex prepared above. The reactor was heated to 60°C and then pressurized to 2.07 MPa with a mixture of 95.0 wt.% TFE and 5.0 wt.% P. A 250 ml aliquot of an aqueous 10 wt.% ammonium persulfate initiator solution was then added. A mixture of 73.0 wt.% TFE, 23.0 wt.% P, and 4.0 wt.% TFP was supplied to

20      the reactor to maintain a pressure of 2.07 MPa throughout the polymerization. The initiator solution was fed continuously at 5 ml/hour through the end of the reaction period. After a total of 6000 g monomer

25

30

mixture had been supplied to the reactor, monomer addition was discontinued and the reactor was purged of residual monomer. The total reaction time was 26 hours. The resulting fluoroelastomer latex was  
5 coagulated by addition of aluminum potassium sulfate solution and then washed with deionized water. The polymer crumb was dried for two days at 60°C. The product, composed of 73 wt.% TFE units, 23 wt.% P units, and 4 wt.% TFP units, was an amorphous fluoroelastomer having a glass transition temperature of 3°C, as determined by differential scanning  
10 calorimetry (heating mode, 10°C/minute, inflection point of transition).  
Mooney viscosity, ML-10 (121°C), was 48.

Control B

A control polymer of the prior art (Control Polymer B) was prepared  
15 by a semi-batch emulsion polymerization, carried out at 60°C in a well-stirred reaction vessel. A 33-liter, horizontally agitated reactor was charged with 20 liters of deionized, deoxygenated water, 200 g of perfluorohexylethyl sulfonic acid and 18 g of sodium hydroxide. The reactor was heated to 60°C and then pressurized to 2.07 MPa with a  
20 mixture of 95.0 wt.% TFE and 5.0 wt.% P. A 326 ml aliquot of an aqueous initiator solution was then added. The solution contained 10 wt.% ammonium persulfate and 3.5 wt.% sodium hydroxide. A mixture of 77.8 wt.% TFE and 22.2 wt.% P was supplied to the reactor to maintain a pressure of 2.07 MPa throughout the polymerization. The initiator solution  
25 was fed continuously at 6 ml/hour through the end of the reaction period. After a total of 8000 g monomer mixture had been supplied to the reactor, monomer addition was discontinued and the reactor was purged of residual monomer. The total reaction time was 14 hours. The resulting emulsion was coagulated by addition of aluminum potassium sulfate  
30 solution and then washed with deionized water. The polymer crumb was dried for two days at 60°C. The product, composed of 78 wt.% TFE units and 22 wt.% P units, was an amorphous fluoroelastomer having a glass

transition temperature of -0.9°C, as determined by differential scanning calorimetry (heating mode, 10°C/minute, inflection point of transition). Mooney viscosity, ML-10 (121°C), was 32.

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Example 7

A curable composition of the invention (Sample 5) was made by mixing a fluoroelastomer of the invention (Polymer 5 prepared above) with a polyhydroxy curative, acid acceptor, vulcanization accelerator and other 10 ingredients on a conventional two-roll rubber mill, using standard mixing techniques employed in the elastomer industry. A comparative curable composition (Comparative Sample C) was made by the same procedure except that a fluoroelastomer of the prior art (Control Polymer B), not containing TFP cure site monomer units was used. The formulations are 15 shown in Table II.

Curing characteristics were measured by MDR (at 177°C, 24 minutes) according to the Test Methods. The results are also shown in Table II. Compression set of ½ inch (1.3 cm) cured (10 minutes at 177°C) pellets was measured according to the Test Methods. Results are 20 included in Table II.

Control Polymer B, which did not contain copolymerized units of TFP cure site monomer, did not cure under these conditions as indicated by the lack of a measurable increase in S' when Comparative Sample C was run in the MDR. On the other hand, Sample 5 which contained a 25 polymer of the invention having copolymerized units of TFP, cured well as shown by the rise in S' and the excellent compression set value for the cured pellet.

TABLE II

<u>Ingredient, phr</u>	<u>Sample 5</u>	<u>Comp. Sample C</u>
Polymer 5	100	0
Control Polymer B	0	100
TBAOH <sup>5</sup>	2.3	2.3
Maglite® D <sup>6</sup>	6	6
Bisphenol AF	2	2
MT Carbon Black	30	30
<u>Curing Characteristics</u>		
S'min, dN·m	0.35	--
S'max, dN·m	10.1	--
tc90, minutes	5.06	--
<u>Compression Set</u>		
Compression Set B, 70 hours @200°C, %	24	--

5       <sup>5</sup> 8.9 ml of a 1.0 M solution of tetrabutylammonium hydroxide in methanol on 3.0g of an inert support of Micro-Cel E synthetic calcium silicate powder, available from World Minerals, Inc.

6       <sup>6</sup> Magnesium oxide available from C.P. Hall

#### Example 8

Curable compositions of the invention (Samples 6 and 7) were  
10 made by mixing a fluoroelastomer of the invention (prepared substantially as Polymer 1 above except containing 76 wt.% copolymerized units of TFE, 20 wt.% units of P and 4 wt.% units of TFP) with a derivative of a polyhydroxy curative, acid acceptor, vulcanization accelerator and other ingredients on a conventional two-roll rubber mill, using standard mixing  
15 techniques employed in the elastomer industry. The formulations are shown in Table III.

Curing characteristics were measured by MDR (at 177°C, 24 minutes) according to the Test Methods and results are shown in Table III.

TABLE III

<u>Ingredient, phr</u>	<u>Sample 6</u>	<u>Sample 7</u>
Polymer	100	100
TBAHS <sup>7</sup>	2.3	2.3
Maglite D	3.0	3.0
Hydroquinone Diacetate	1.15	0
Resorcinol Monobenzoate	0	2.14
MT Carbon Black	30	30
Calcium Hydroxide	6.0	6.0
<u>Curing Characteristics</u>		
Tmin, dN·m	0.62	0.59
Tmax, dN·m	12.7	20.43
tc90, minutes	11.45	8.35

<sup>7</sup> n-tetrabutylammonium hydrogensulfate

5    Example 9

Curable compositions of the invention (Samples 8 - 12) were made by mixing a fluoroelastomer of the invention (prepared substantially as Polymer 1 above except containing 73 wt.% copolymerized units of TFE, 23 wt.% units of P and 4 wt.% units of TFP) with various quaternary ammonium salts of bisphenol AF (1:1 molar ratio), acid acceptor, and other ingredients on a conventional two-roll rubber mill, using standard mixing techniques employed in the elastomer industry. The formulations are shown in Table IV.

10      Curing characteristics were measured by ODR (at 177°C, 3° arc, 12 minutes) according to the Test Methods and results are shown in Table IV.

TABLE IV

<b>Ingredient, phr</b>	<b>Sample 8</b>	<b>Sample 9</b>	<b>Sample 10</b>	<b>Sample 11</b>	<b>Sample 12</b>
Polymer	100	100	100	100	100
TMAHAF <sup>8</sup>	2.54	0	0	0	0
TPrAHAf <sup>9</sup>	0	3.21	0	0	0
MTBAHAF <sup>10</sup>	0	0	3.15	0	0
TBAHAF <sup>11</sup>	0	0	0	3.45	0
TPeAHAf <sup>12</sup>	0	0	0	0	3.78
Elastomag 170	3	3	3	3	3
Calcium hydroxide	6	6	6	6	6
MT carbon black	30	30	30	30	30
<u>Curing characteristics</u>					
M <sub>L</sub> , dN·m	7.5	4.4	3.6	4.4	3.8
M <sub>H</sub> , dN·m	9.8	81.9	70.6	51.2	22.8
t <sub>s2</sub> , minutes	--	4.0	3.8	4.4	--
tc90, minutes	--	13.7	7.6	19.3	--

<sup>8</sup> tetramethylammonium/BPAF salt (1:1 molar ratio)<sup>9</sup> tetrapropylammonium/BPAF salt (1:1 molar ratio)5      <sup>10</sup> methyltributylammonium/BPAF salt (1:1 molar ratio)<sup>11</sup> tetrabutylammonium/BPAF salt (1:1 molar ratio)<sup>12</sup> tetrapentylammonium/BPAF salt (1:1 molar ratio)